

Microresonators in Titanium Nitride

New design and KID properties

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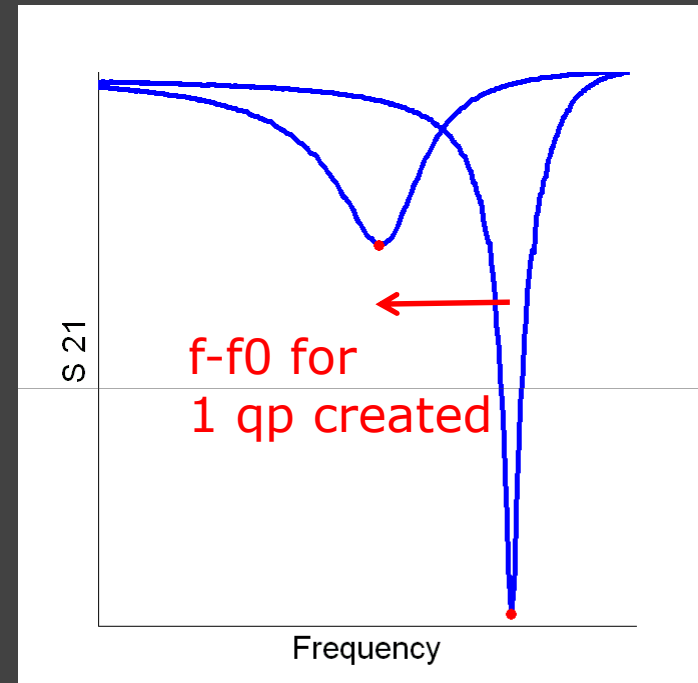
Netherlands Organisation for Scientific Research (NWO)

Why using high resistive material for KIDs ?

$$L_s \approx \hbar \rho / \pi \Delta t$$

$$\delta (f-f_0)/f_0 / \delta N_{qp} \propto L_s / (L_g + L_s)$$

Ex: Al KIDs 50nm: $f-f_0 \sim 0.1\text{Hz} / \text{qp}$



Why Titanium Nitride ?

Leduc et al. APL 2010

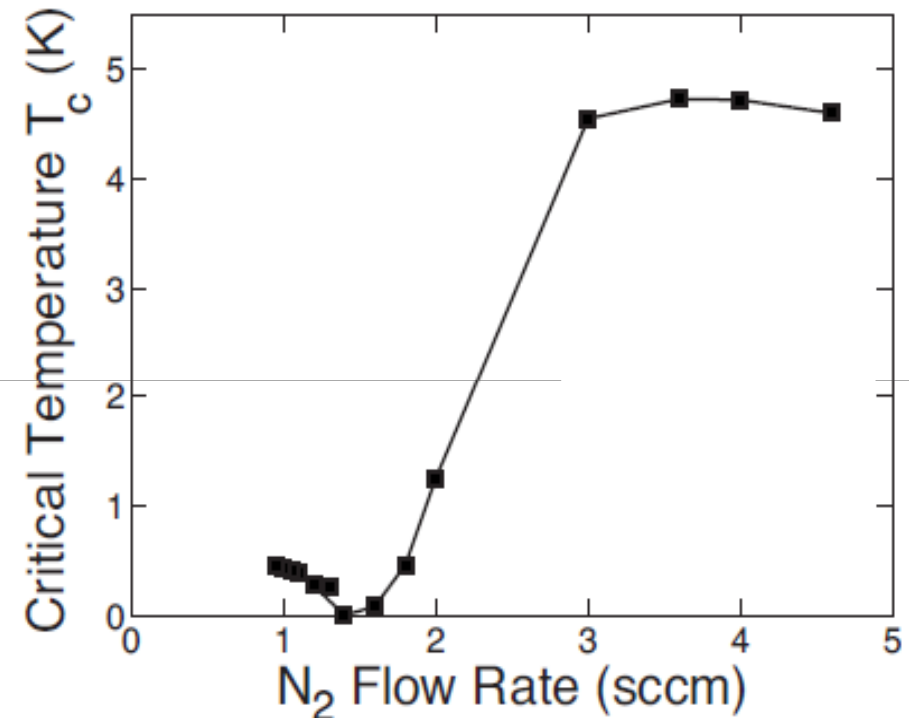
$$L_s \approx \hbar \rho / \pi \Delta t$$

TiN – film used here:
 $\rho \approx 130 \mu\Omega\text{cm}$
 $T_c = 0.8\text{K} \rightarrow \Delta = 125 \mu\text{eV}$

$\rightarrow L_s \approx 44 \text{ pH}$

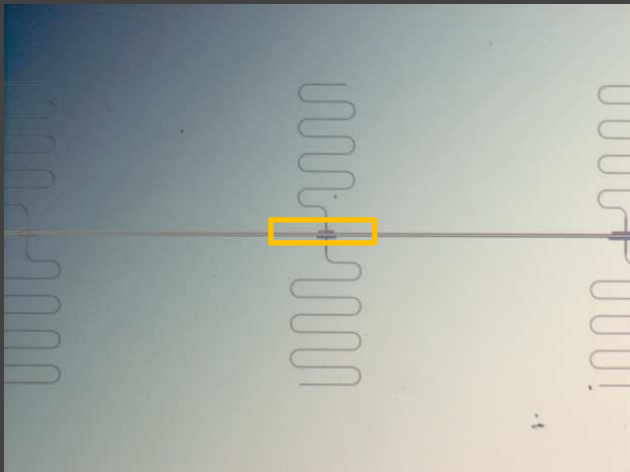
(Aluminum : $L_s < 0.1 \text{ pH}$)

T_c change with N_2 content

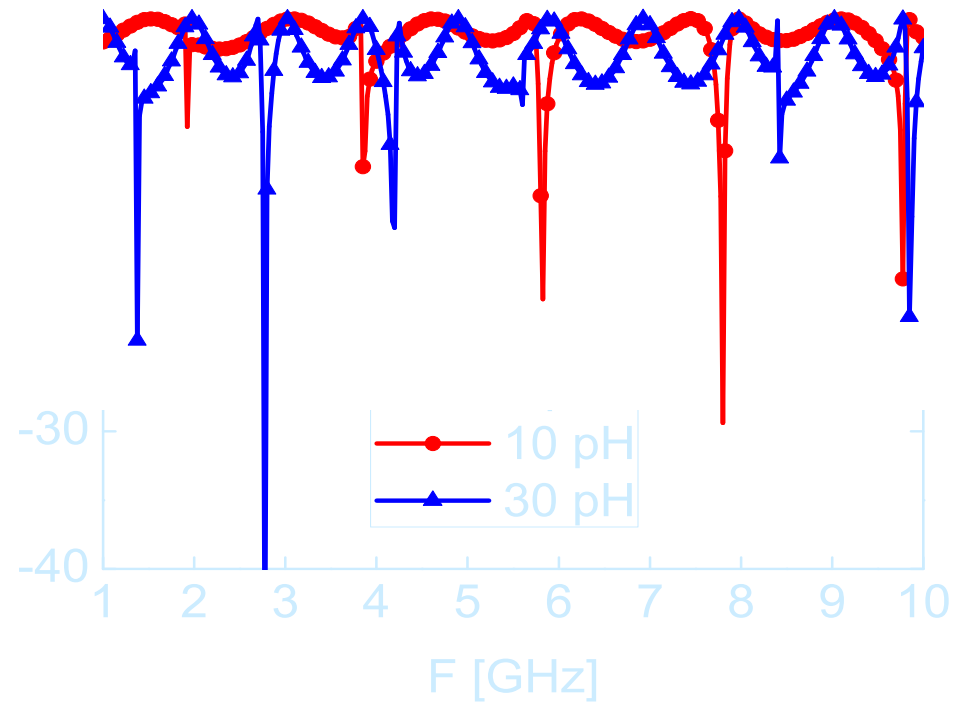


Microwave design need to be adapted

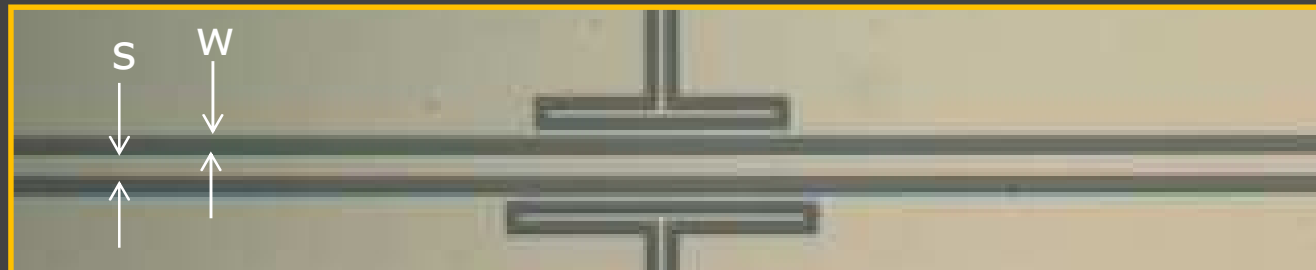
For a typical (Al) chip



PARASITIC DIP IN THE CHIP TRANSMISSION

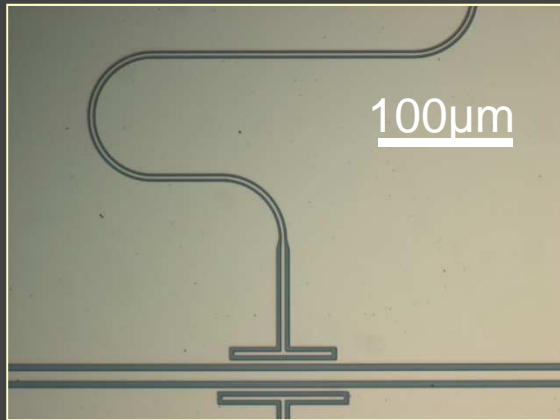


With
 $s=10\mu\text{m}$
 $w=6\mu\text{m}$

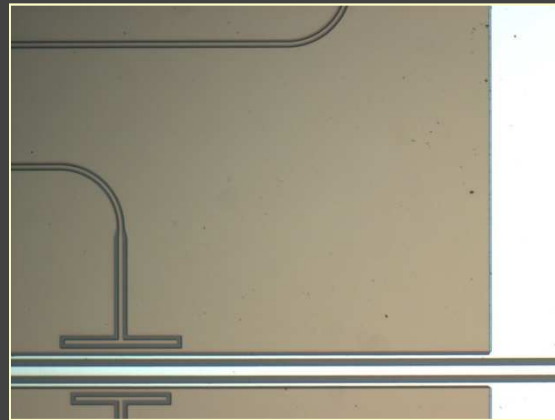


New hybrid design : KIDs TiN / Throughline Al

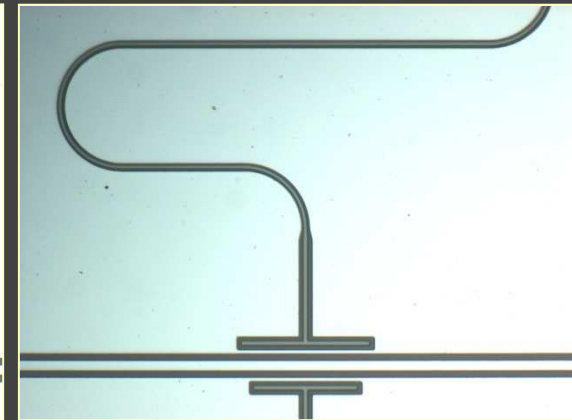
(to compare) Mono



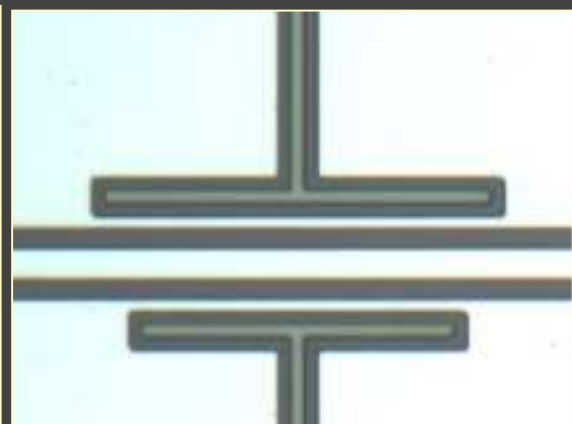
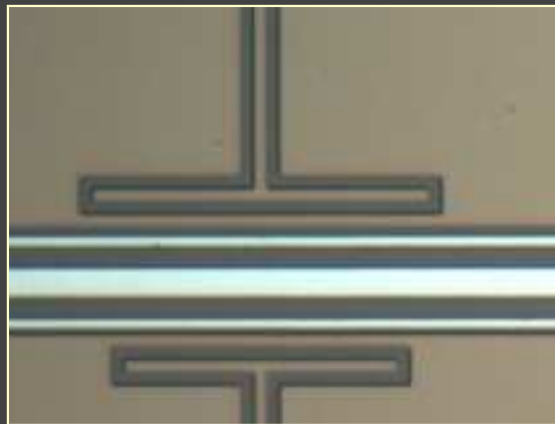
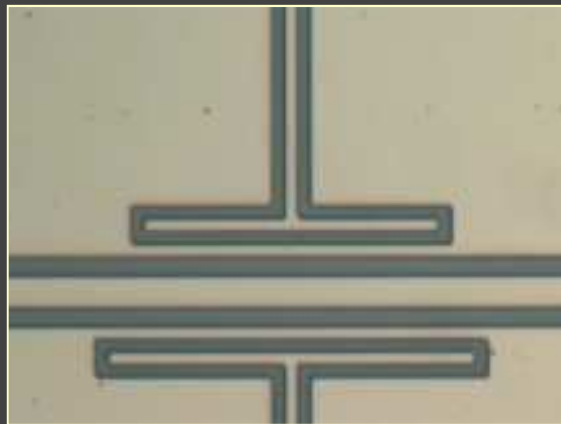
(hybrid) Duo



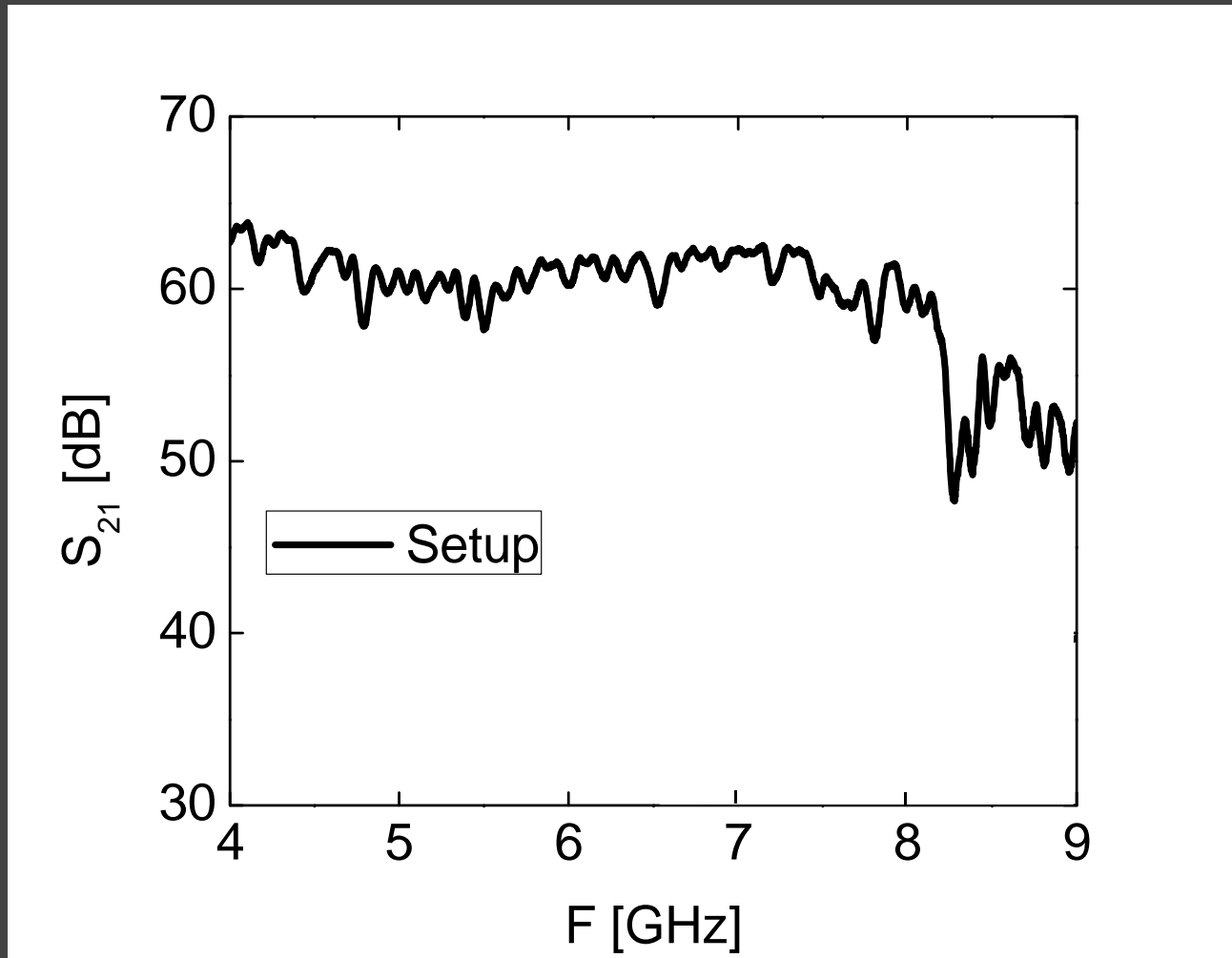
(Hybrid) KIDmix



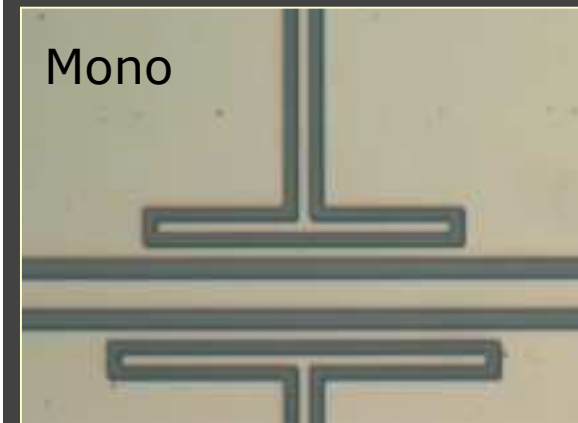
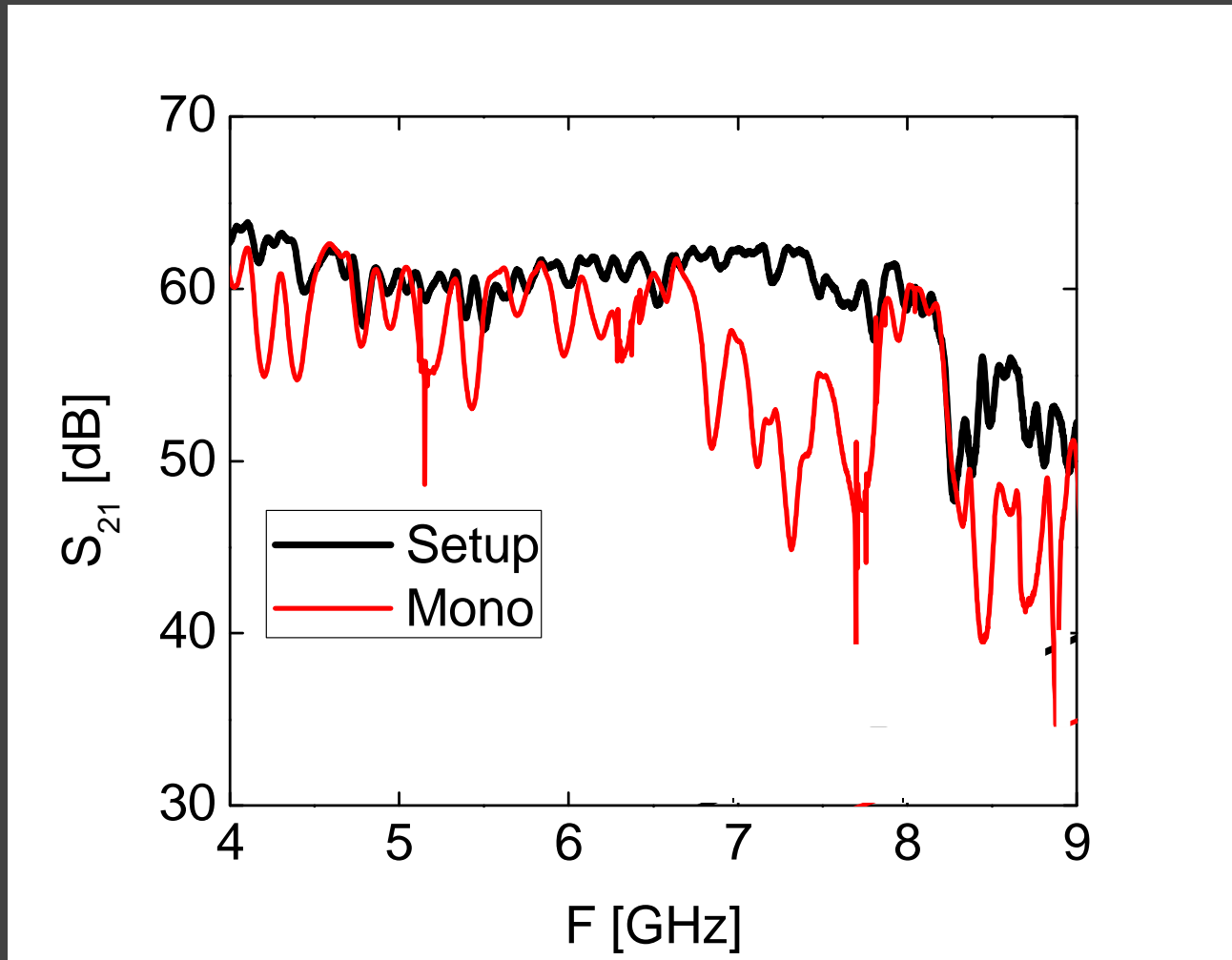
Zoom x3:



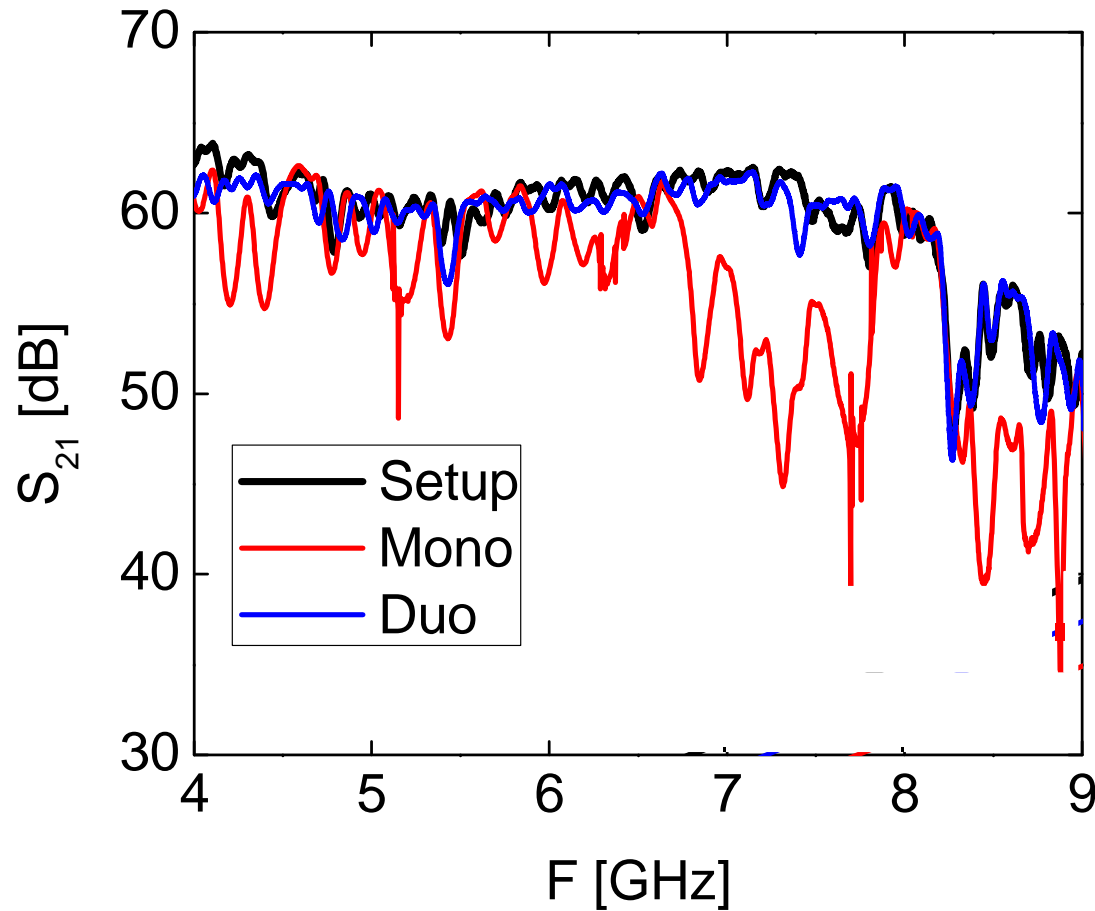
Lossless S21 transmission in the Hybrid designs



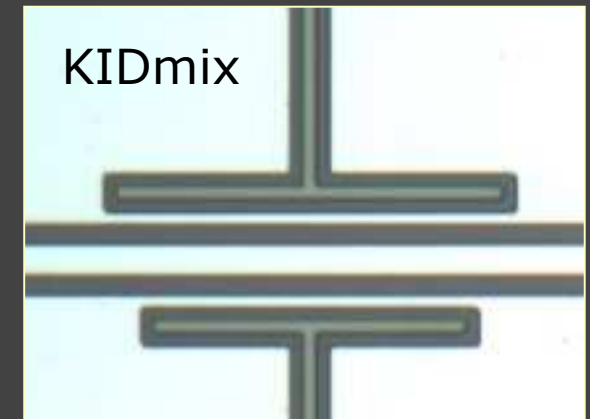
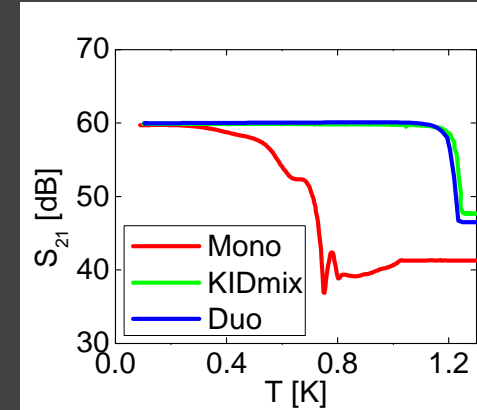
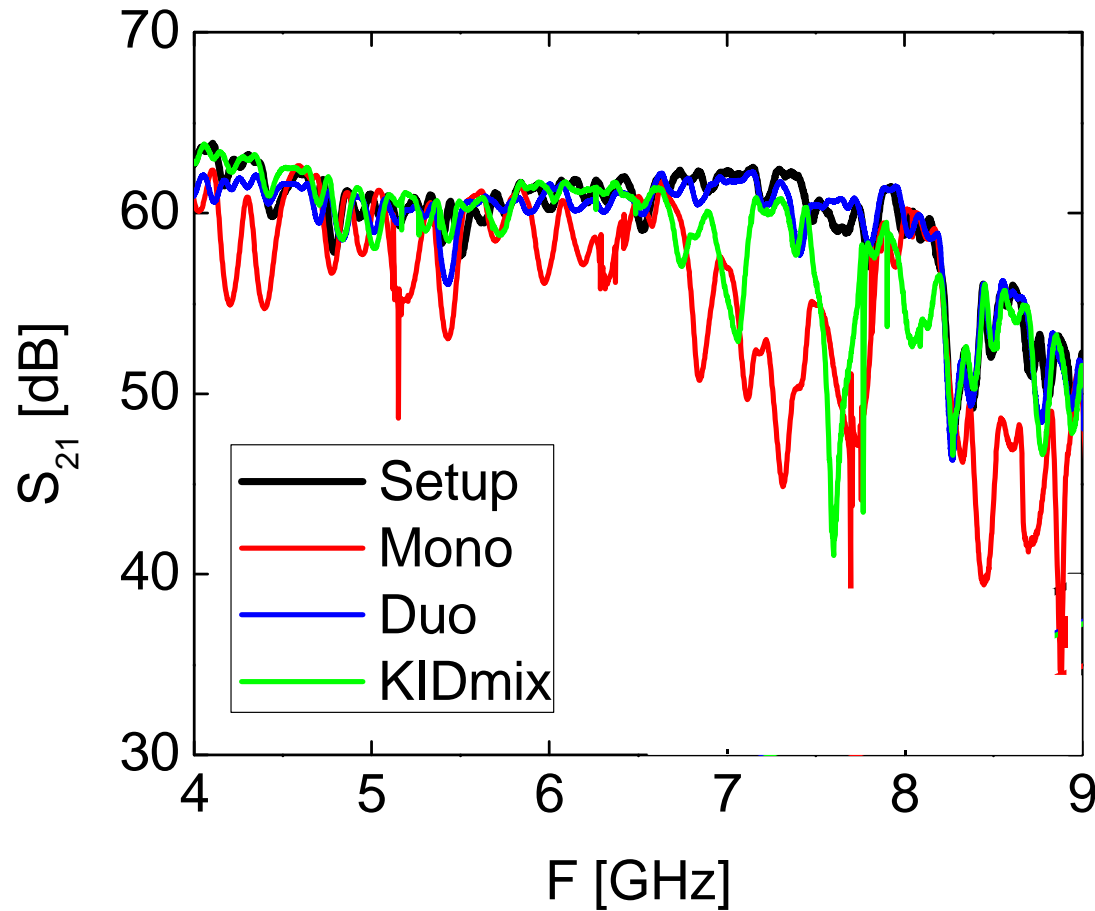
Lossless S21 transmission in the Hybrid designs



Lossless S21 transmission in the Hybrid designs

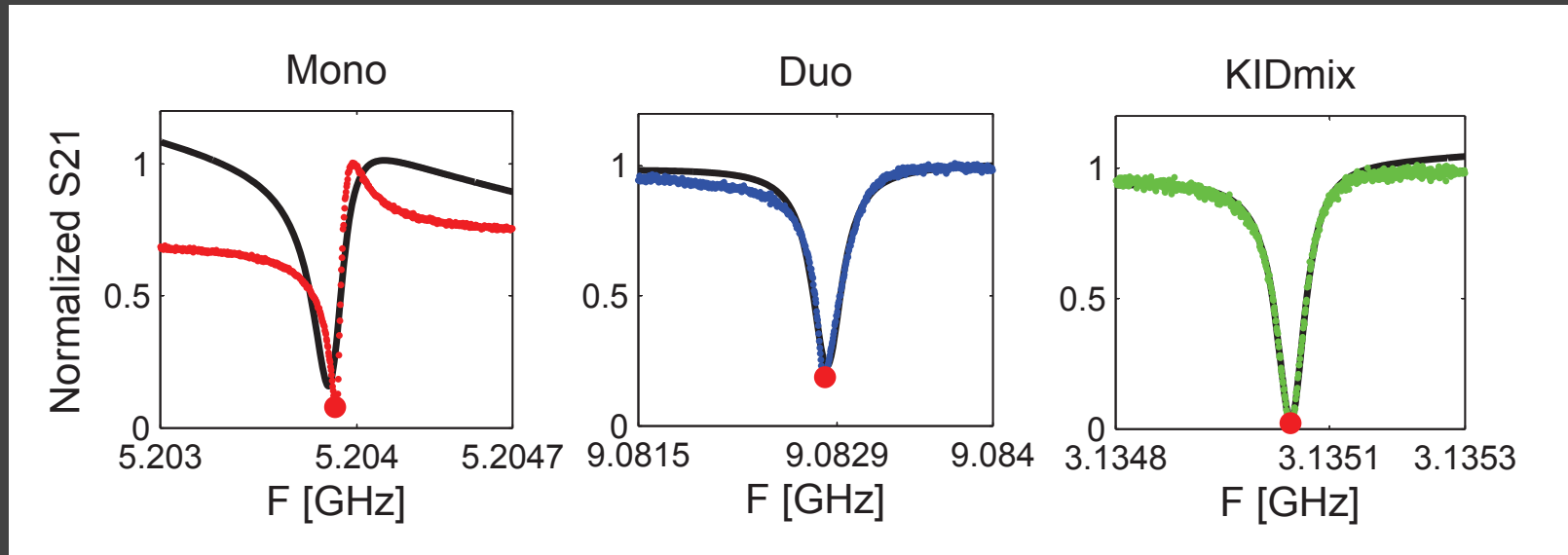


Lossless S21 transmission in the Hybrid designs



$f_{\text{exp}}/f_{\text{geom}} = 0.2 \rightarrow \alpha = 96\%$

KID dips

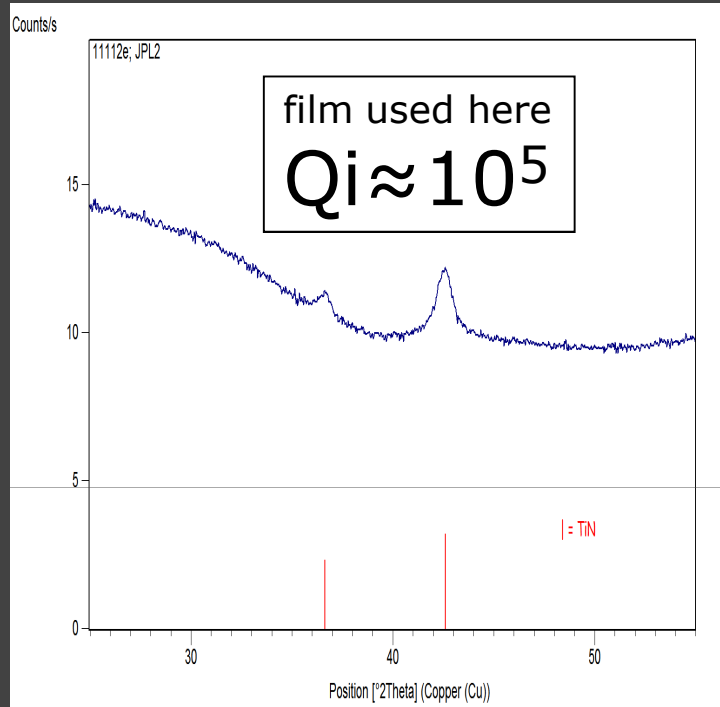


$$Q_i = 2 \cdot 10^5$$

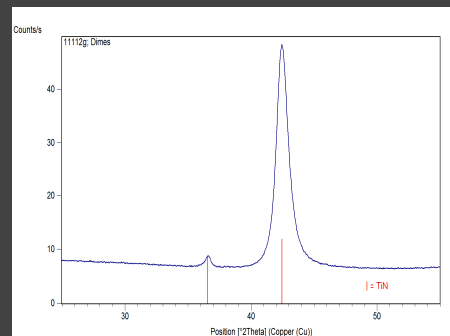
$$Q_i = 9 \cdot 10^4$$

$$Q_i = 5 \cdot 10^5$$

Note on Qi and crystalline orientation - by XRD



film from
DIMES/Delft
 $Q_i \approx 10^7$



Vissers et al.

Appl. Phys. Lett. 97, 232509 (2010)

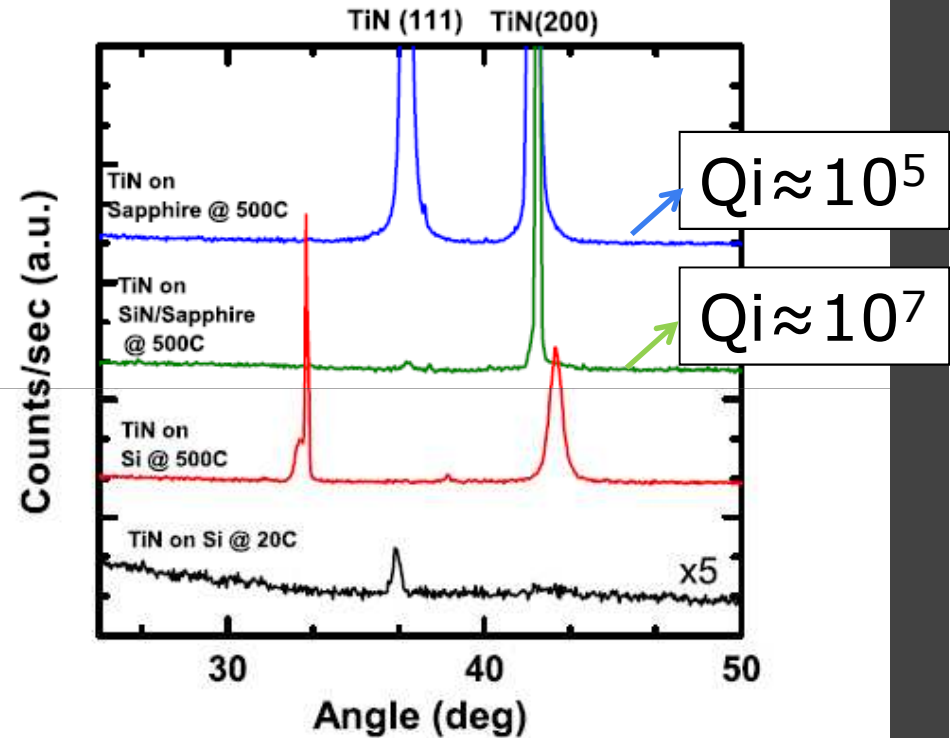
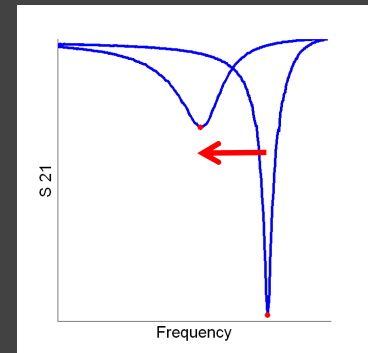


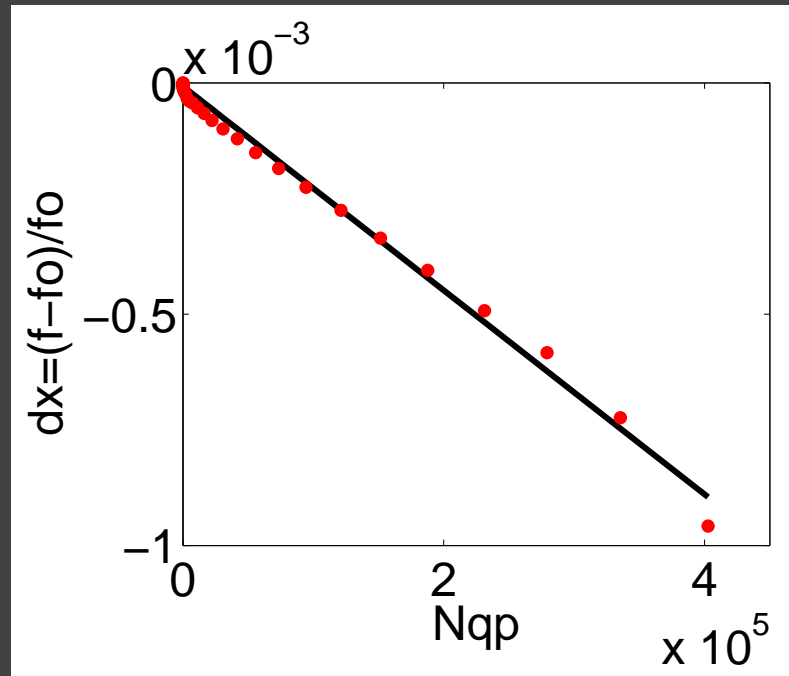
FIG. 2. (Color online) θ - 2θ XRD scans of TiN films on sapphire, Si and SiN/Si at 500 °C, and Si at 20 °C. The (111)-TiN peak at $2\theta=36^\circ$ is present on the sapphire substrate as well as for Si room temperature. The TiN grown at high temperature on Si and SiN both exhibit primarily (200)-TiN peak at 2θ around 42° . The sharp peak at 33° on high temperature TiN on Si is due to the XRD being performed on a patterned sample with exposed Si regions.

Large responsivity

$$N_{qp}(T) = 2V N_0 \sqrt{2\pi k_B T \Delta} \exp\left(-\frac{\Delta}{k_B T}\right)$$



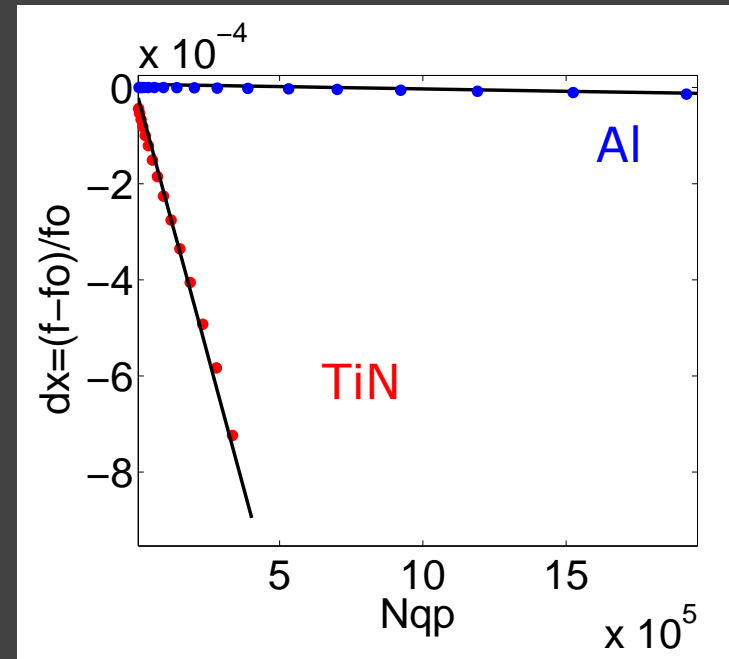
TiN T_c=1K



$f - f_0 \sim 10 \text{ Hz} / qp$

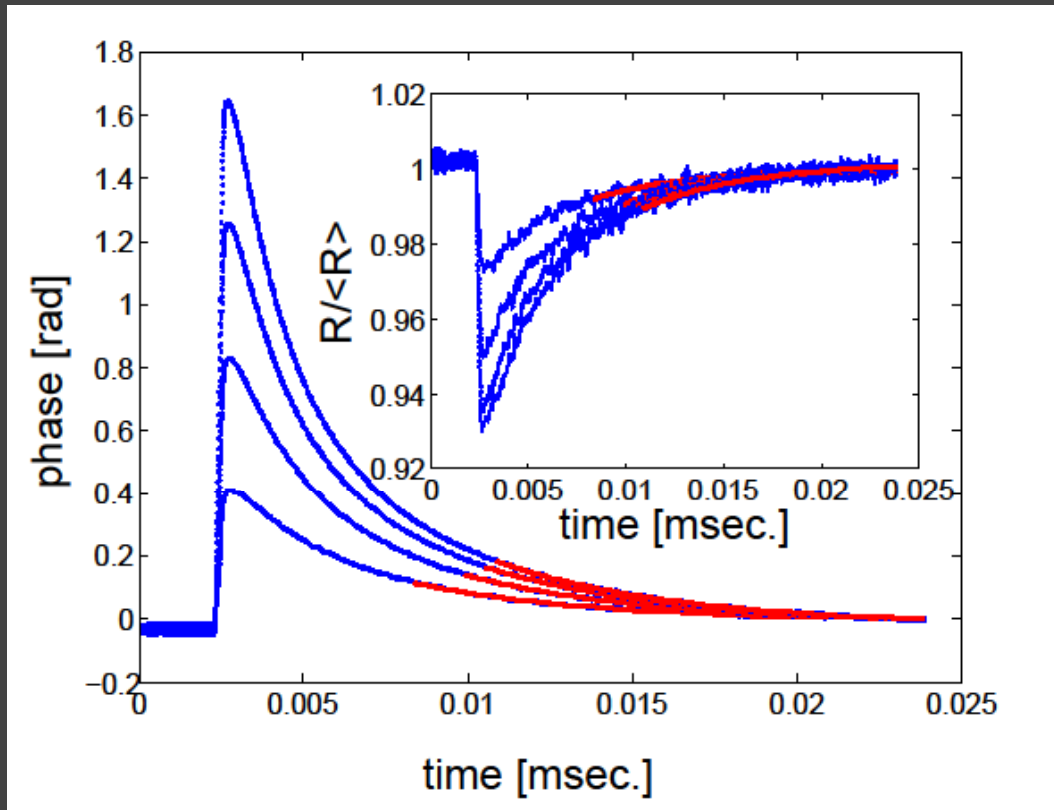
$(dx / dN_{qp} = 2.2 \times 10^9)$

Comparison with Al

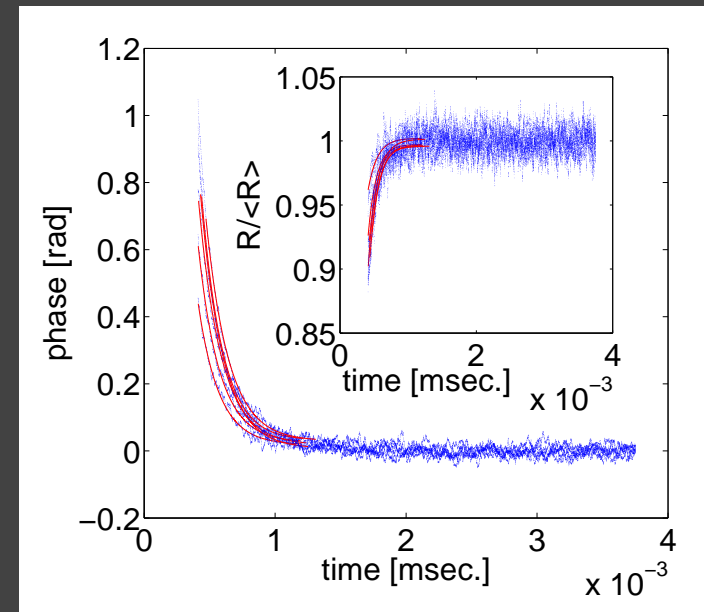


$f - f_0 \sim 0.1 \text{ Hz} / qp$

Lifetime



As high as 5.6 ms

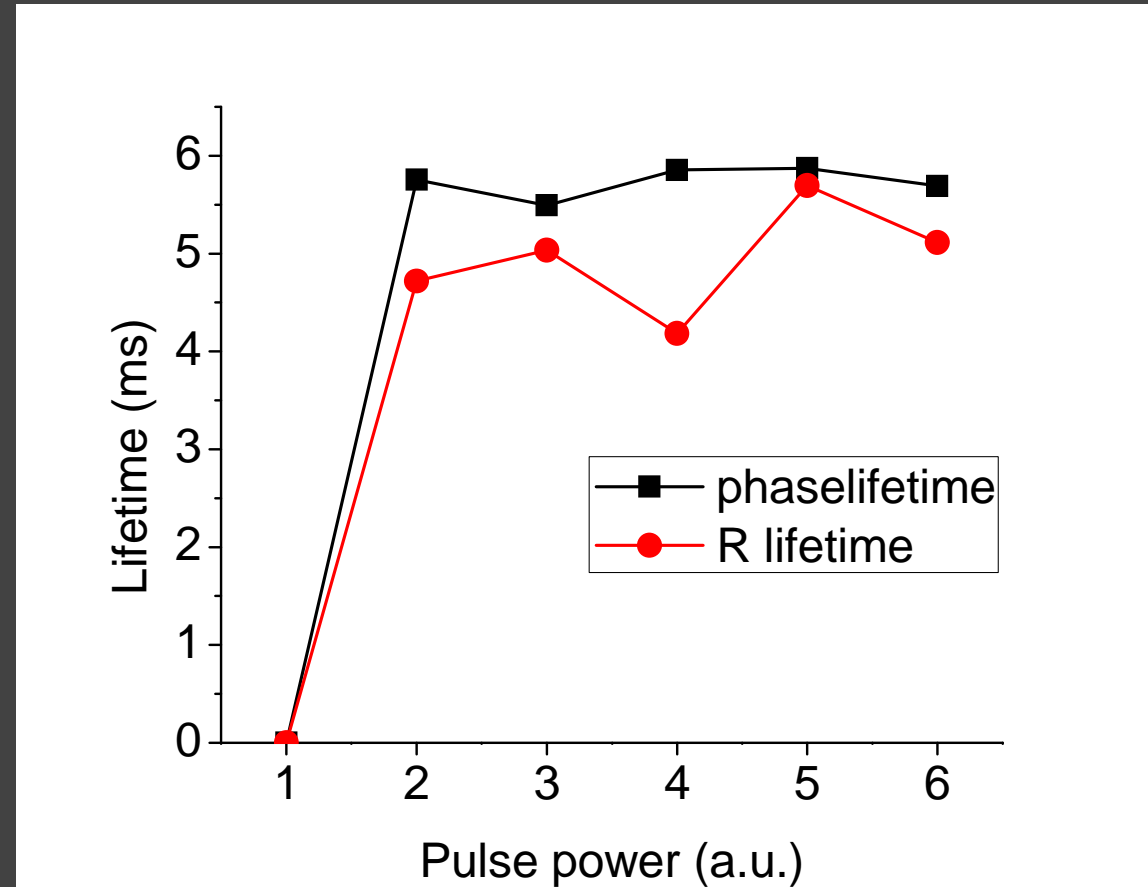
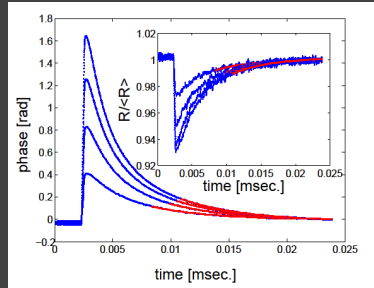


$\tau = 0.17$ ms

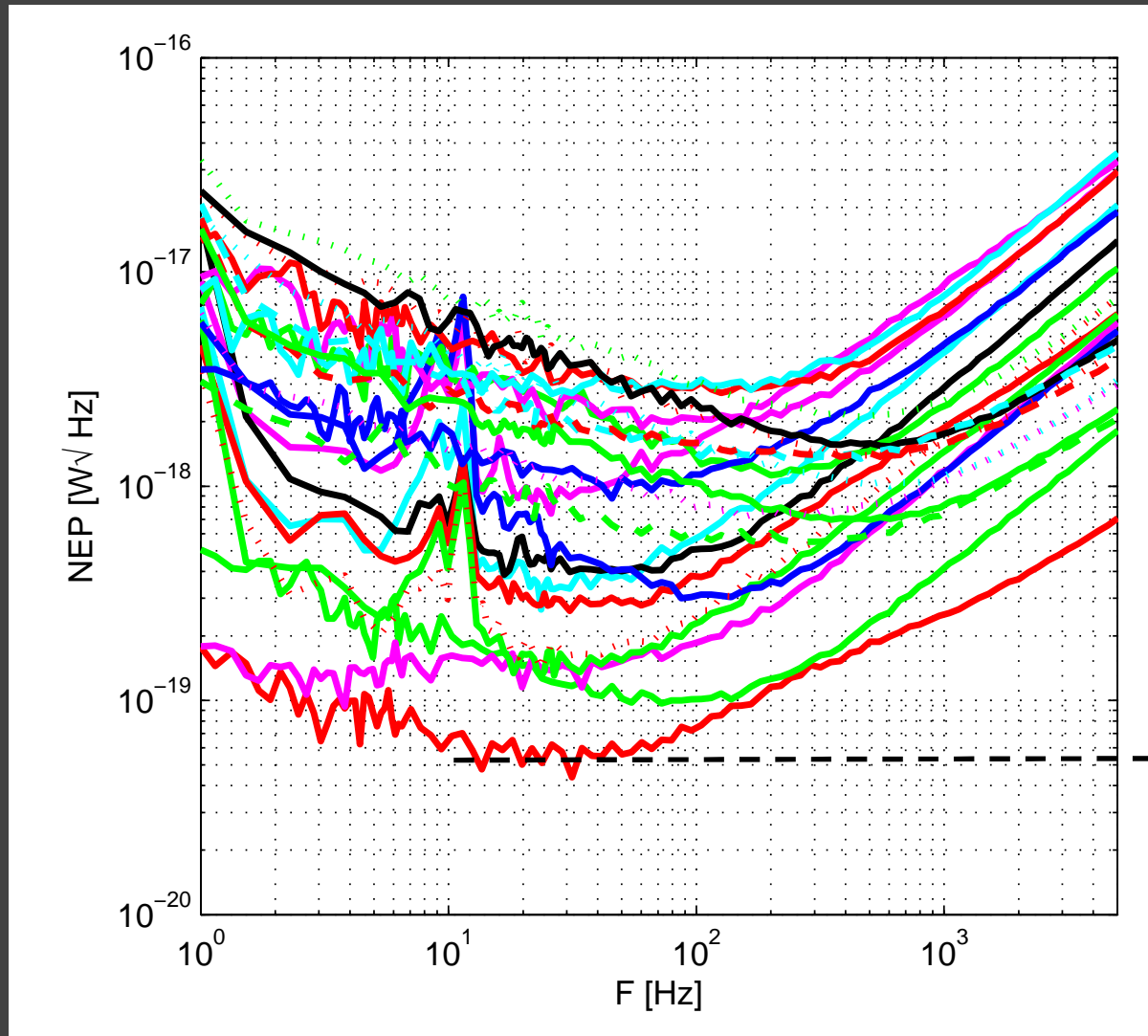
But large variations between KIDs

Lifetime

Check of the data giving $\tau = 5.6$ ms

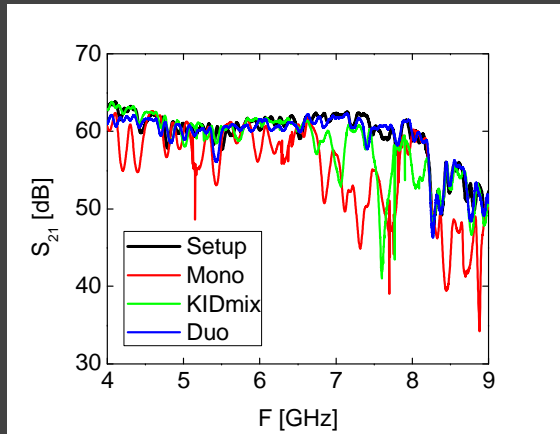


Electrical NEP (in phase)

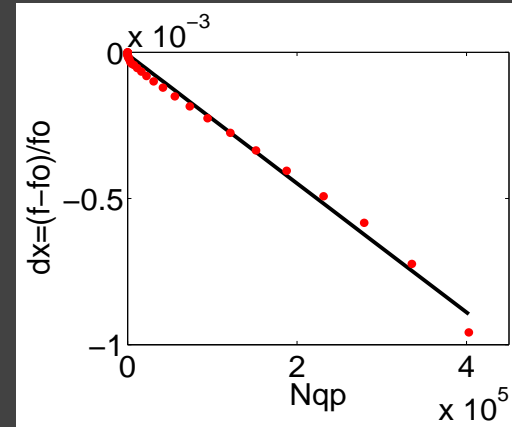


Best NEP :
 $4 \times 10^{-20} \text{ W}\sqrt{\text{Hz}}$

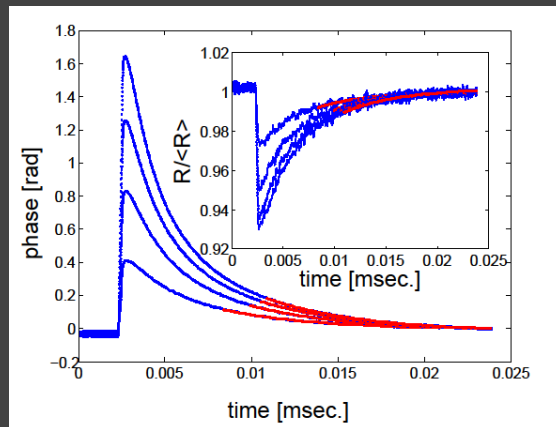
Conclusions



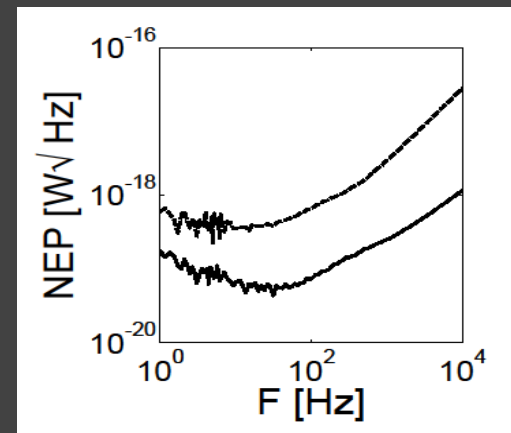
New design



Large
responsivity



Lifetime up
To 5.6 ms



Best NEP :
 4×10^{-20} W/\sqrt{Hz}

Collaboration

SRON

Jochem Baselmans
Steve Yates
Jan-Joost Lankwarden

JPL

Rick Leduc
Loren Swenson for the KISS group

TU Delft

Pieter-Jan Coumou
Hugo Schellevis
Akira Endo
Teun Klapwijk

Cardiff U.

Simon Doyle
Julie Gould

Example of NEP calculation for the best KID

following the classical analysis described in [Baselmans&al J Low Temp Phys (2008) 151: 524-529]

$$NEP_{\theta} = \frac{\sqrt{S_{\theta}}}{\left(\frac{\eta\tau}{\Delta} \frac{\delta\theta}{\delta x} \frac{\delta x}{\delta N_{qp}}\right)} (1 + \omega^2\tau^2)(1 + \omega^2\tau_{res}^2)$$

$S_{\theta} = -63dBc/Hz = 10^{-63/10}rad^2/Hz$ noise, measured at 100Hz, 100mK, with optimal power -102dBm (purple curve)

$\eta = 0.57$ efficiency of quasiparticle creation

$\tau = 3.68ms$ quasiparticle lifetime, measured at 100mK

$\Delta = 125\mu eV = 2.00 \cdot 10^{-23}J$ superconducting gap, from $\Delta = 1.81k_B T_c$ [Escoffier&al PRL 2004] and $T_c = 0.8K$ measured in this chip with S21(T)

$\frac{\delta\theta}{\delta x} = \frac{4Q}{f_0}$ with $Q = 2.91 \cdot 10^{-4}$ the measured (loaded) quality factor and $f_0 = 5.20GHz$ the KID frequency at 100mK

$$x(T) = \frac{f(T) - f_0}{f_0}$$

$\frac{\delta x}{\delta N_{qp}} = -2.21 \cdot 10^{-9}$ linear fit between 100 and 200mK of the measured frequency response. T is translated to N_{qp} via the relation:

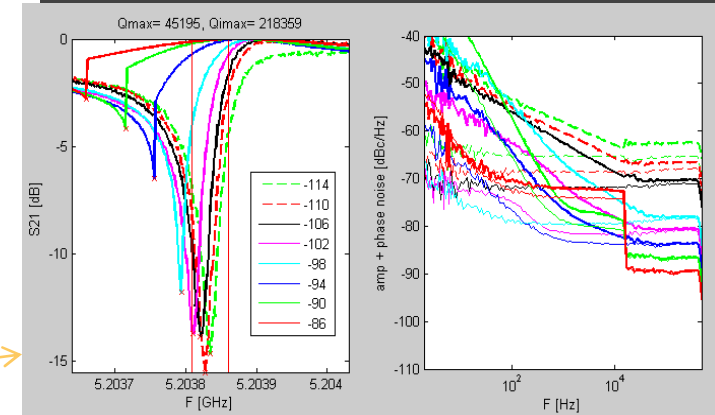
$N_{qp}(T) = 2VN_0\sqrt{2\pi k_B T \Delta} \exp\left(-\frac{\Delta}{k_B T}\right)$ with $V = 4056\mu m^2 \times 50nm$ the volume of the resonator and $N_0 = 8.7 \cdot 10^9 eV^{-1} \mu m^{-3}$ from [Leduc&al APL 2010]

$(1 + \omega^2\tau^2)(1 + \omega^2\tau_{res}^2)$ frequency cut off due to the qp and resonator ring time - can be neglected here

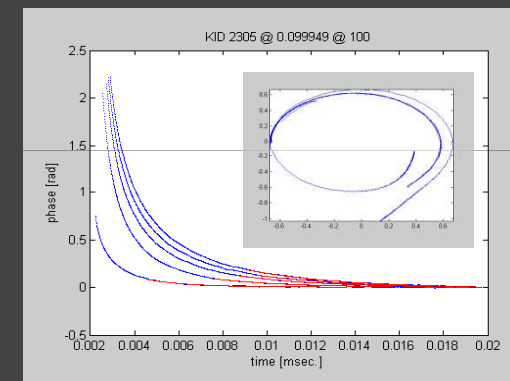
Putting all together:

$$NEP_{\theta} = 5 \cdot 10^{-20} W \sqrt{Hz}$$

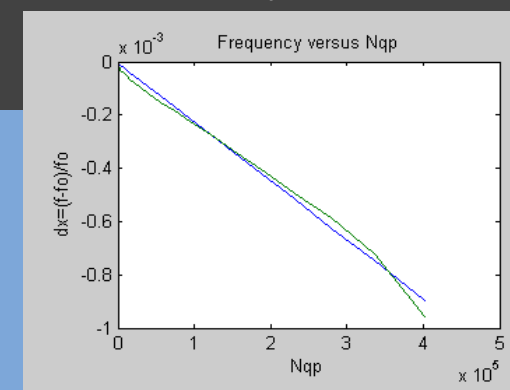
S_{θ} measurement



Lifetime



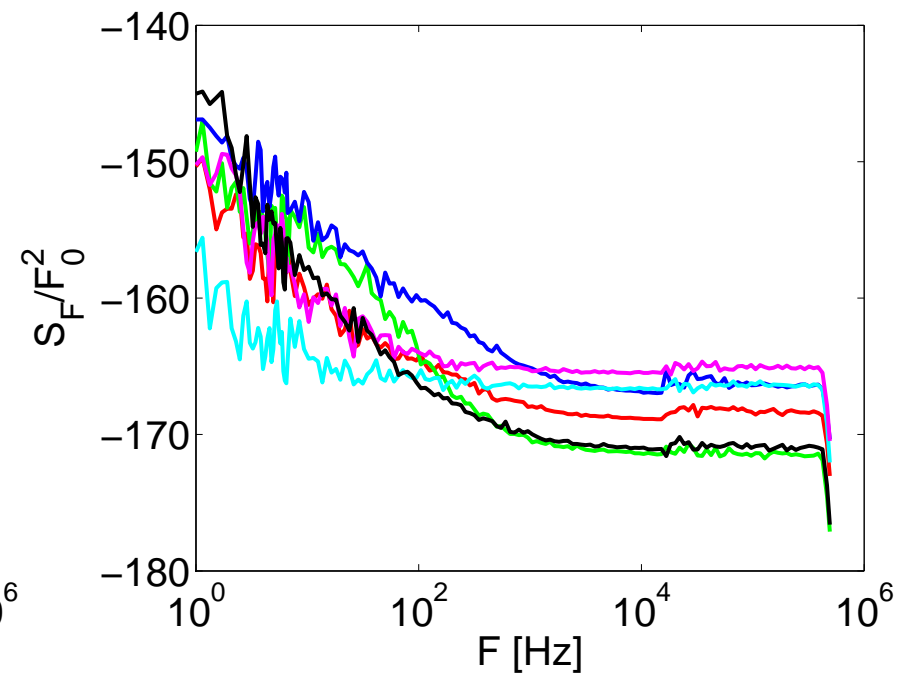
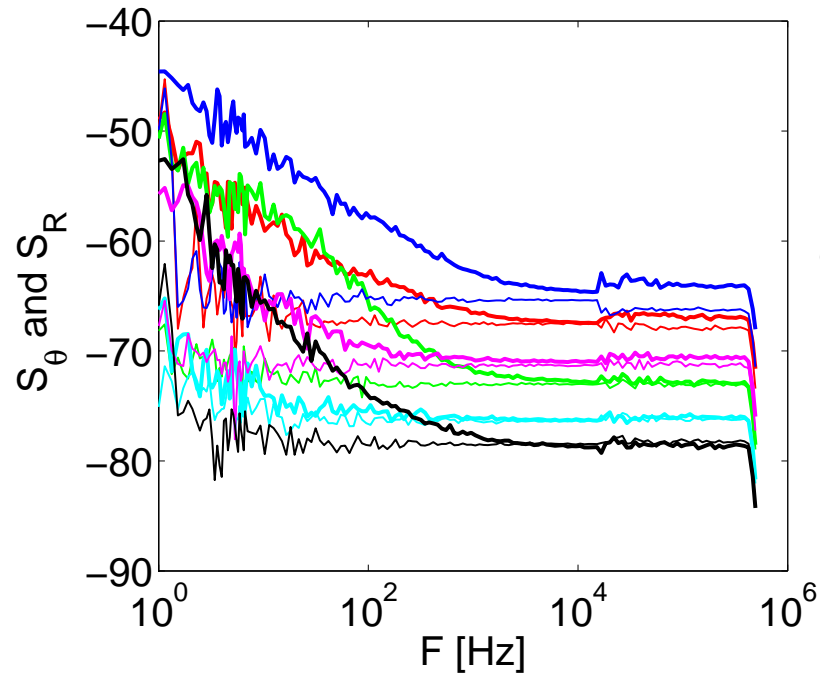
Frequency response



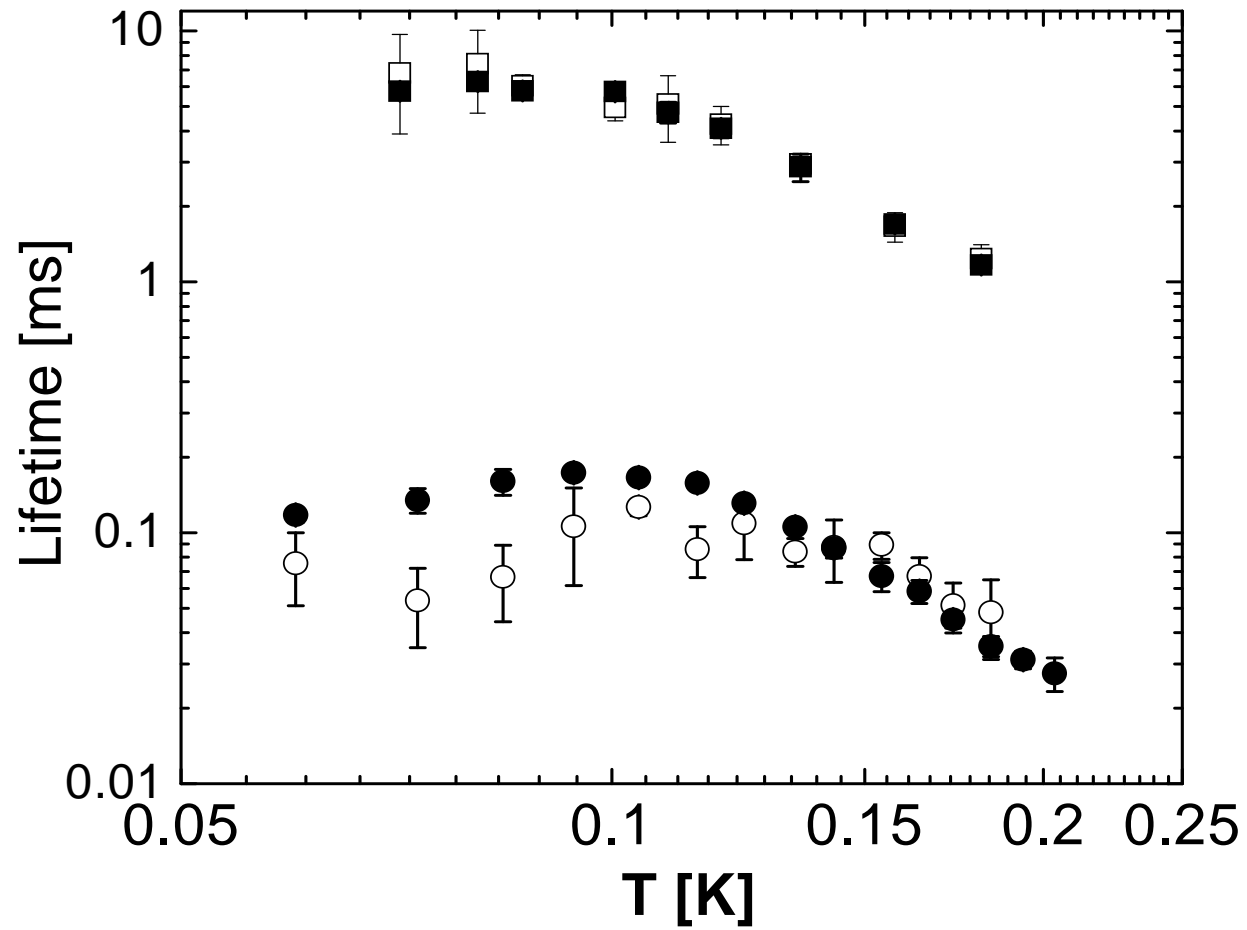
(WVO)

Noise

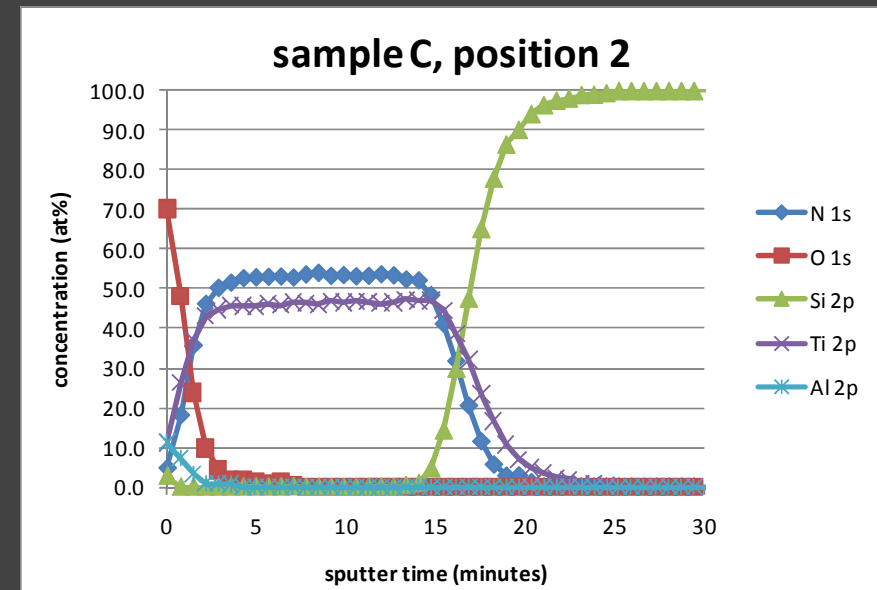
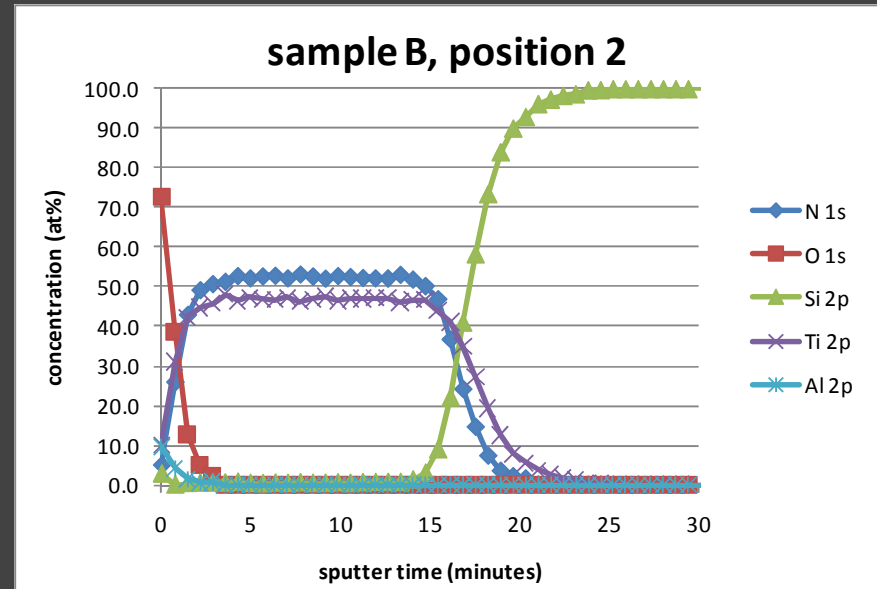
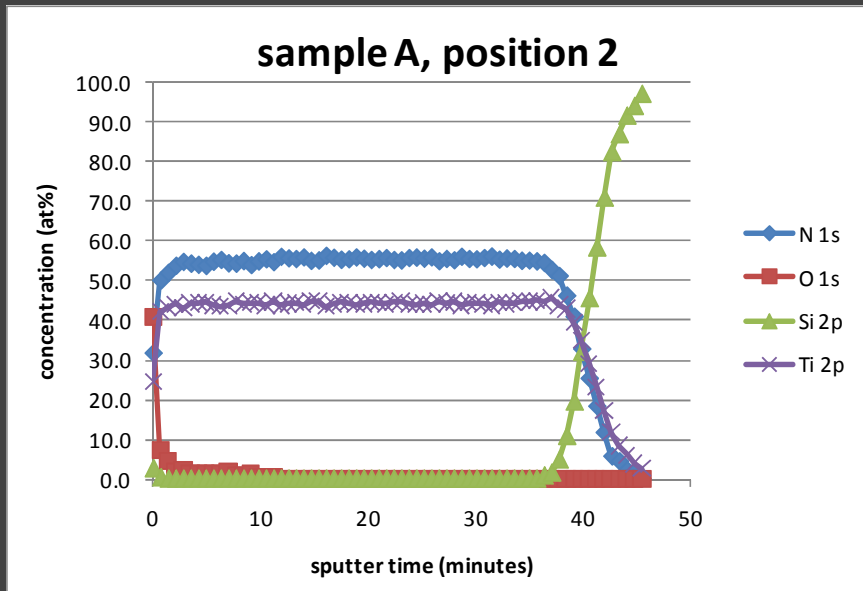
(in Duo)



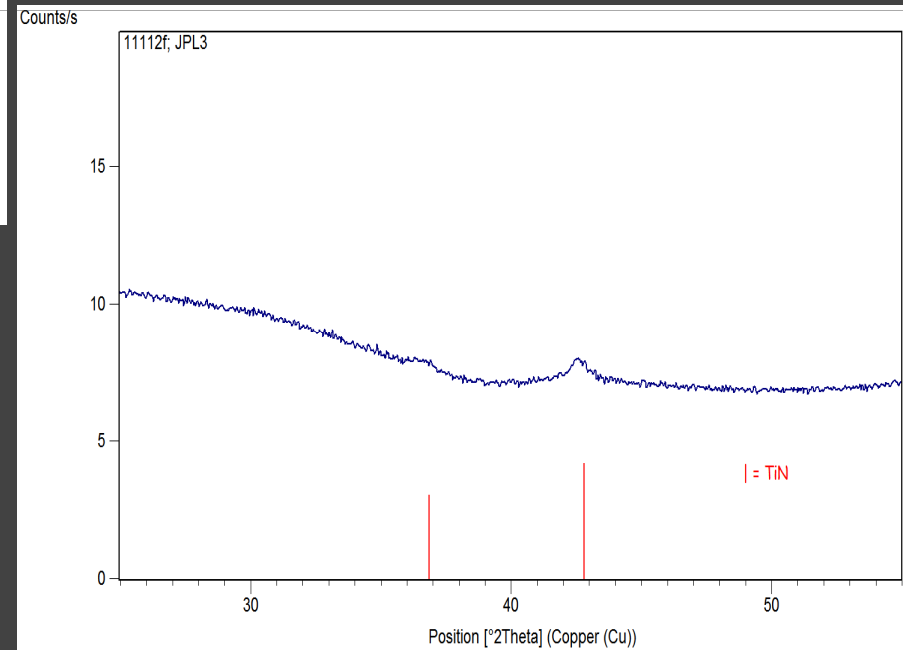
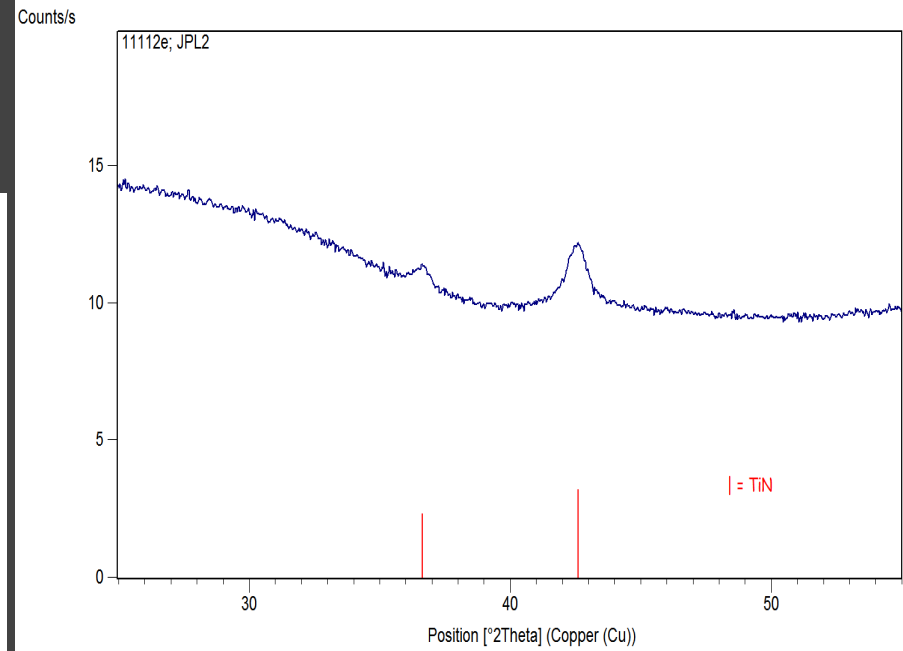
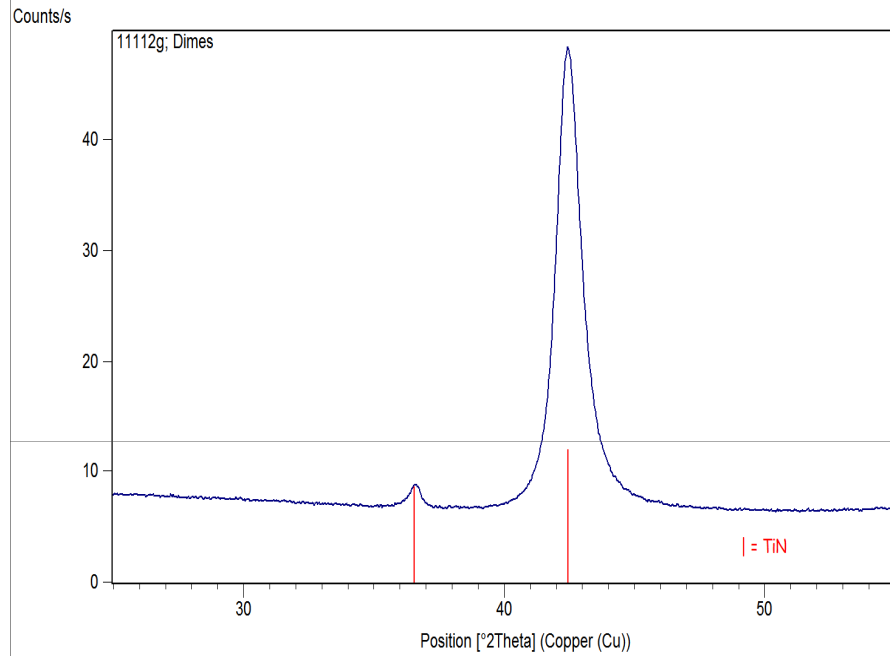
Lifetime 3



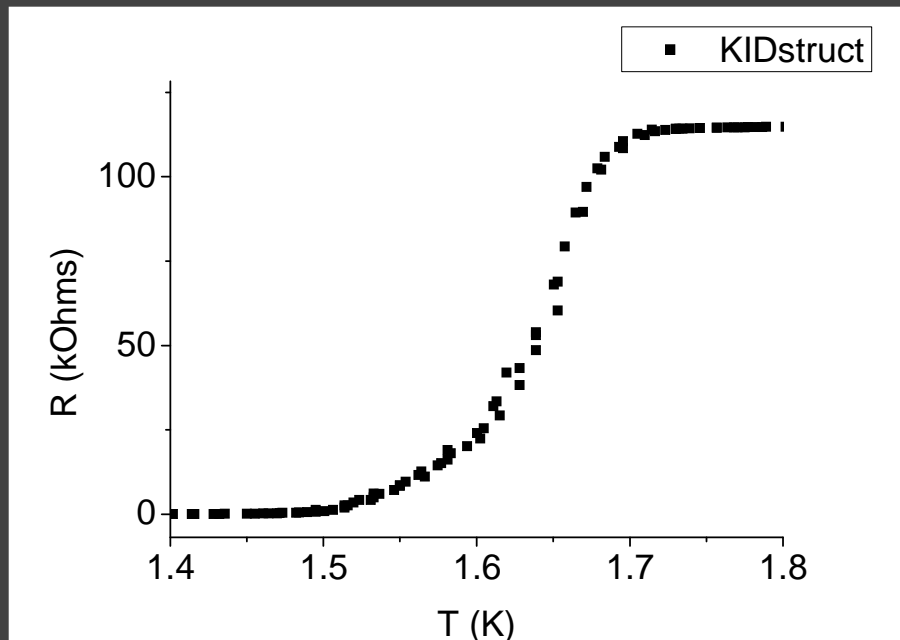
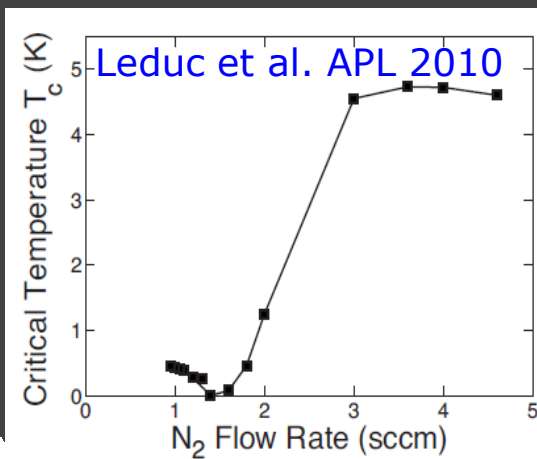
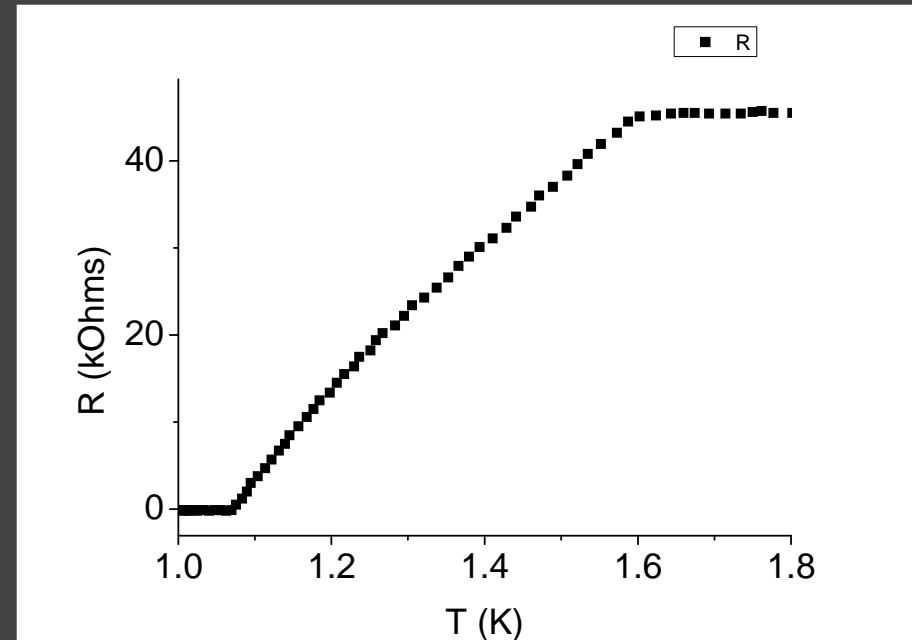
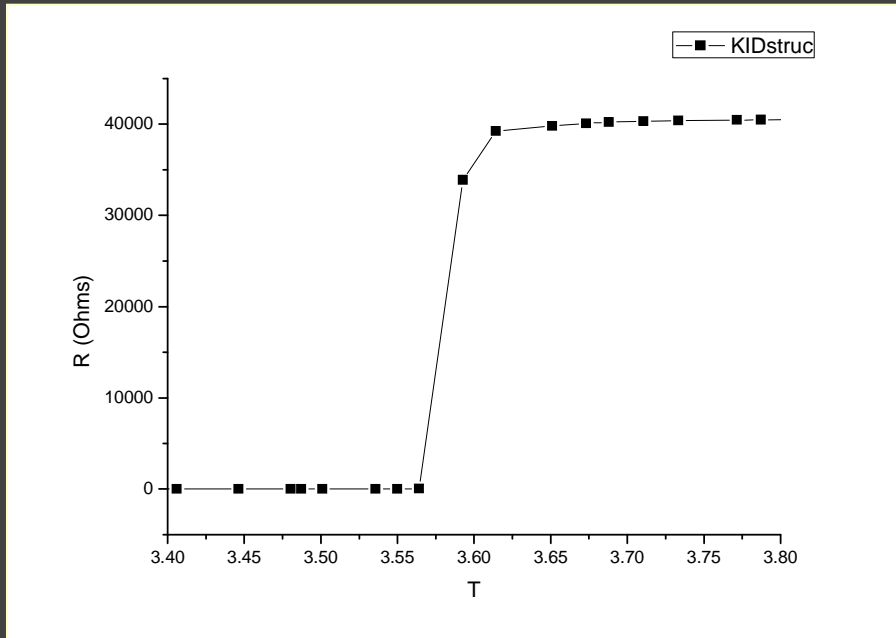
Internal Q factor 2



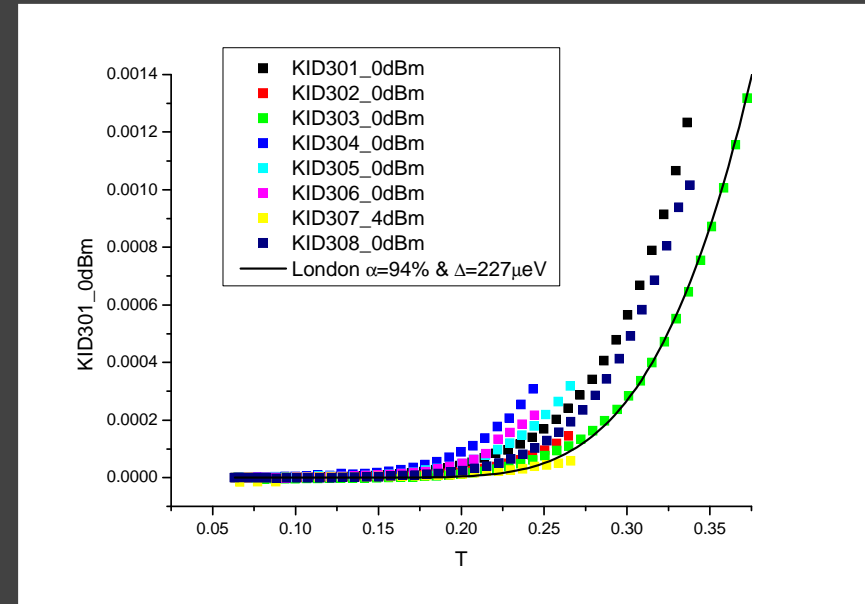
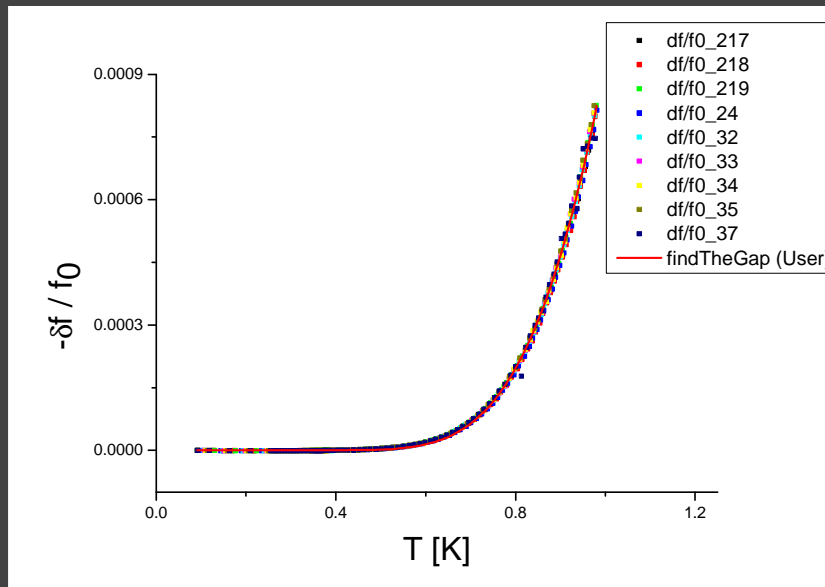
Internal Q factor 4



Internal Q factor 1



Responsivity 1



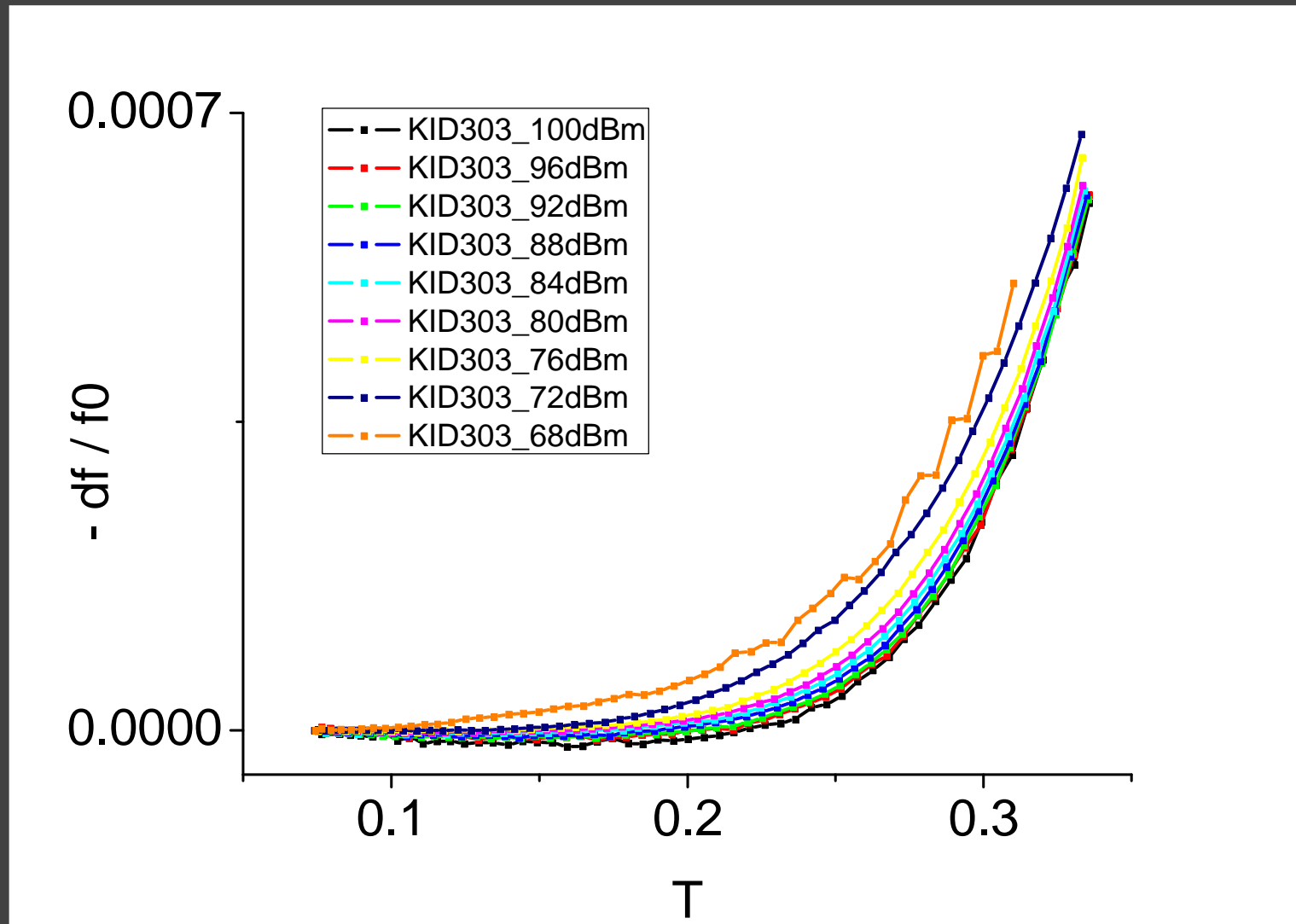
Gap=0.57meV (6.67K)

$T_c=3.6$ K

\rightarrow gap/k $T_c=1.85$

Escoffier&al PRL04: gap/ $T_c=1.81$ (STM/S meas.)

Responsivity 2



LeKIDs designs for optical chips – Simon Doyle

